## Transmission and Distribution of Electrical Power

By
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Lecture (1)

## Syllabus

1 - Introduction.
2 - Fundamentals of Electrical Power Engineering.
3 - Transmission Line Constants Calculation.
4 - Transmission Line Models and Calculations.
5 - Mechanical Design of Overhead Transmission Line.

- D.C. Power Transmission Technology.
- Overhead Line Insulator.
- Corona
- Underground Cables

10 - Electrical Power Distribution

## Marks Distribution Chart



## Engineering Definition

## What is Engineering?

Engineering is the application of math and science by which properties of matter and the sources of energy in nature are made useful.

## Engineering Design Definition

## What is Design?

## So, Engineering design is.........

## Applications \& Examples

## Why Engineering Design?

## Betterment of society through



Design


Manufacturing


Research \& Development


Management


Continual Improvement


## Engineer Definition

## Who is Engineer?

## Creative

Iterative


Integrated

Innovation is the key Oven Story!!!!!!!!!!

## So, Engineer is.........

## Engineering Process Cycle

The engineering process cycle is achieved by following 10 stages.
1-Identify the problem/product innovation
2-Define the working criteria/goals
3-Research and gather data
4-Brainstorm / generate creative ideas
5-Analyze potential solutions

## Engineering Process Cycle

6-Develop and test models.
7-Make the decision.
8-Communication and specify.
9-Implement and commercialize.
10-Perform post-implementation review and assessment.

$$
\begin{gathered}
\text { Electricity } \\
\text { Changes } \\
\text { Cifestyce }
\end{gathered}
$$

## Six key questions

- 


## What is the electrical energy?

How do we produce electric energy?

## Why do we think the electrical energy is important?

## What are the resources of electrical energy?

## What about renewable energy resources?

What about the concept of smart grid?

## TYPES Of Power plants

## Hydroelectric Power Plants



## Hydroelectric Power Plants

*Advantages of hydroelectric power plant
*Disadvantages of hydroelectric power plant



## Steam Power Plants

*Advantages of Steam Power Plants

## *Disadvantages of Steam Power Plants



## Solar Power Plants



## *Theory of operation

## Solar Power Plants

## *Advantages of Solar Power Plants

*Disadvantages of Solar Power Plants


## Diesel Power Plants



## *Theory of Operation

## Diesel Power Plants

*Advantages of Diesel Power Plants
*Disadvantages of Diesel Power Plants


## Gass turbine Power Plants



> *Theory of operation

DIAGRAM OF TYPICALLARGE GAS TURBBE

## Gas turbine Power Plants

*Advantages of
Gas-turbine Power Plants
*Disadvantages of Gas-turbine Power Plants


## Nuclear Power Plants



*Theory of Operation

## Nuclear Power Plants

*Advantages of nuclear power plant
*Disadvantages of nuclear power plant


## Contents

*Chapter 1:
Transmission Line Constants
*Chapter 2:
Transmission Line Models and Calculations

* Chapter 3:

Mechanical Design of Overhead T.L
*Chapter 4:
D.C. power Transmission Technology

## Chapter 1: Transmission Line Constants

1. Main parts of over head T.L.


Ground

## Types of conductors

* Hard -drawn copper conductors.

Aluminum- core steel-rein forced (ACSR).

* For rural electrification , all - aluminum conductors are used.
* Steel wires are used as earthing wires for over head T. L.

The main constants required are

* Resistance ( R "ohm" ).
* Inductance ( L "hennery") \& corresponding $X_{L}$.
* Capacitance (C" farad ") \& corresponding $X_{c}$.


## Resistance of oxer head

* $\mathrm{R}=\rho \mathrm{L} / \mathrm{A} \quad \Omega$
*Where :
R: resistance of T.L ( $\Omega$ )

$\rho$ : resistivity of T.L conductor ( $\Omega$.m )
L : length of T.L (m)
A: cross -section area ( $\mathrm{m}^{2}$ )
*For hard -drawn conductors : $\rho=1.724^{* 1} 10^{-8} \Omega . \mathrm{m}$ at $20^{\circ} \mathrm{C}$
*For all-aluminum conductors : $\rho=2.860^{* 1} 10^{-8} \Omega$.m at $20^{\circ} \mathrm{C}$


## Effect of Temperature on Ressistance

* The resistance of T.L increases with Temperature
* The rise in resistance depends on the Temperature coefficient of conductor material (a).

$$
\frac{R_{t 2}}{R_{t 1}}=\frac{1 / \alpha_{0}+t_{2}}{1 / \alpha_{0}+t_{1}}
$$

Where :
$\mathrm{R}_{\mathrm{t} 2}$ : Resistance of T.L at $\mathrm{t}_{2}$
$\mathrm{R}_{\mathrm{t} 1}$ : Resistance of $\mathrm{T} . \mathrm{L}$ at $\mathrm{t}_{1}$
$\mathrm{a}_{0}$ : Temperature coefficient at $0^{\circ} \mathrm{C}$

$\mathrm{T}_{1}$ : First temperature
$\left({ }^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{2}$ : Second temperature

* For hard - drawn copper For aluminum

$$
\begin{align*}
& a_{0}=0.0041^{\circ} / \mathrm{C}  \tag{}\\
& \mathrm{a}_{0}=0.0038^{\circ} / \mathrm{C}
\end{align*}
$$

when alternating current is passing through conductors, there is an unequal distribution of current in any cross - section of the conductor, the current density at the surface being higher than the current density at the center of the conductor . this causes larger power loss for a given r.m.s alternating current than the loss when the same value of DC is flowing in the conductor.
${ }^{*} R_{\mathrm{ac}}>\mathrm{R}_{\mathrm{dc}}$

$$
\begin{aligned}
& \mathrm{R}_{\mathrm{ac}}=\frac{\text { Average power losses }}{\mathrm{I}^{2}{ }_{\mathrm{rms}}} \\
& \text { Skin effectratio }=\frac{\mathrm{R}_{\mathrm{ac}}}{\mathrm{R}_{d c}}
\end{aligned}
$$

## Which depends on

* Permeability (Type of material).
* Area of cross section of the conductor.
* Frequency of the supply.


## Inductance \& Reactance of O.H.T.L

## Inductance of overhead transmission line depends

 on:*Size of conductor. *Distance between conductors. *Material of conductors.

## Inductance \& Reactance of O.H.T.L

$$
\mathrm{H}=\frac{I}{2 \pi x}
$$

A.turn/m

H: electric field intensity.

$$
\begin{array}{rl}
\mathrm{B}=\frac{2 * 10^{-7}}{x} I & \mathrm{wb} / \mathrm{m}^{2} \\
\mathrm{H}=\frac{I x}{2 \pi r^{2}} & \text { A.turn } / \mathrm{m}
\end{array}
$$



$$
B=\frac{2 * 10^{-7}}{r^{2}} I x
$$

$\mathrm{wb} / \mathrm{m}^{2}$

## Inductance of Two Conductor (Single Phase)

$\lambda_{\text {total }}=\lambda_{\text {inside }}+\lambda_{\text {outside }}$

$$
\begin{aligned}
& \lambda_{\text {inside }}=\int_{0}^{r} \frac{2 * 10^{-7} x I}{r^{2}} * \frac{\pi x^{2}}{\pi r^{2}} d x \\
& \lambda_{\text {inside }}=\int_{0}^{r} \frac{2 * 10^{-7} x^{3}}{r^{4}} d x=\left.\frac{2 * 10^{-7} I}{r^{4}} \frac{1}{4} x^{4}\right|_{0} ^{r}
\end{aligned}
$$

$$
=\frac{2 * 10^{-7} I}{4 r^{4}} * r^{4}=\frac{1}{2} * 10^{-7} I
$$

## Continue

$$
\begin{aligned}
\lambda_{\text {outside }} & =\int_{r}^{D} \frac{2 * 10^{-7} x I}{r^{2}} * \frac{\pi r^{2}}{\pi x^{2}} d x \\
& =\int_{r}^{D} \frac{2 * 10^{-7 I}}{X} d x=2 * 10^{-7} I \ln \frac{D}{r} \\
\lambda_{\text {outside }} & =2 * 10^{-7} I \ln \frac{D}{r} \quad \text { linkages } / \mathrm{m} \\
\lambda_{\text {total }} & =\lambda_{\text {inside }}+\lambda_{\text {outside }} \\
& =\frac{1}{2} * 10^{-7} I+2 * 10^{-7} I \ln \frac{D}{r}
\end{aligned}
$$

## Continue

$$
\mathrm{L}_{1}=\quad \frac{\lambda_{1}}{I}=10^{-7}\left(2 \ln \frac{D}{r}+\frac{1}{2}\right) \mathrm{H} / \mathrm{m}
$$

## In case of non magnetic or hollow conductor

$$
L_{t}=L_{1}+L_{2}=2 L_{1} \text { ( Two identical conductors ) }
$$

## In Case of Magnetic Conductor

$L=1 \mathrm{O}^{-7}\left(\ln \frac{D}{r}+\frac{1}{2} \frac{\mu}{\mu_{\mathrm{o}}}\right)$
$\mu$ : permeability
$\mu_{r}$ : relative permeability
$\mathrm{X}_{\mathrm{t}}=2 \pi f L_{t} \quad \Omega$
$\lambda=10^{-7} I\left(2 \ln \frac{D}{r}+\frac{1}{2}\right)=2 * 10^{-7} I\left(\ln \frac{D}{r}+\frac{1}{4}\right)$

## Continue

$\lambda=2 * 10^{-7} I \ln \frac{D}{r e^{-0.25}}$
Where:
re ${ }^{-.025}$ : geometric mean radius (GMR ) or self - geometric mean distance.

D : distance bet. Two conductors or mutual distance between two conductors

## General Expression for Inductance of a Group of Parallel Wires

$$
\begin{aligned}
\lambda_{a}=10^{-7}\left(\frac{I_{a}}{2} \frac{\mu}{\mu_{0}}\right. & \left.+2 I_{a} \ln \frac{D_{a x}}{r}\right) \\
\lambda_{\text {total }}=10^{-7}\left(\frac{I_{a}}{2} \frac{\mu}{\mu_{0}}\right. & +2 I_{a} \ln \frac{D_{a x}}{r} \\
& +2 I_{p} \ln \frac{D_{b x}}{D_{a b}} \\
& \left.+. .+2 \ln \ln \frac{D_{n x}}{D_{a n}}\right)
\end{aligned}
$$

$$
I_{n}=-\left(I_{a}+I_{b}+I_{c}+\ldots \ldots . .+I_{n-1}\right)
$$

## Continue

$$
\begin{aligned}
& \begin{aligned}
& \begin{aligned}
\mathrm{a}= & 10^{-7}\left[\frac{\mathrm{I}_{\mathrm{a}}}{2} \frac{\mu}{\mu_{0}}\right.
\end{aligned}+2 \mathrm{I}_{\mathrm{a}}\left(\ln \frac{\mathrm{D}_{\mathrm{ax}}}{\mathrm{r}}-\ln \frac{\mathrm{D}_{\mathrm{nx}}}{\mathrm{D}_{\mathrm{an}}}\right) \\
&+ 2 \mathrm{I}_{\mathrm{b}}\left(\ln \frac{\mathrm{D}_{\mathrm{bx}}}{\mathrm{D}_{\mathrm{ab}}}-\ln \frac{\mathrm{D}_{\mathrm{nx}}}{\mathrm{D}_{\mathrm{ab}}}\right) \\
&\left.+\ldots \ldots . .+2 \mathrm{I}_{\mathrm{n}-1}\left(\ln \frac{\mathrm{D}_{\mathrm{nx}}}{\mathrm{D}_{\mathrm{an}}}\right)\right]
\end{aligned} \\
& \operatorname{since}, \ln A-\ln B=\ln \frac{A}{B}
\end{aligned}
$$

## Continue

$$
\begin{aligned}
\lambda_{a}=10^{-7}\left[\frac{I_{a}}{2} \frac{\mu}{\mu}\right. & +2 I_{a}\left(\ln \frac{D_{a x}}{r} \cdot \frac{D_{a n}}{D_{n x}}\right) \\
& +2 \operatorname{II}\left(\ln \left(\frac{D_{b x}}{D_{a b}} \cdot \frac{D_{a n}}{D_{n x}}\right)\right) \\
& \left.+\ldots+2 I_{n-1}\left(\ln \left(\frac{D_{n-1 x}}{D_{a n-1}} \cdot \frac{D_{a n}}{D_{n x}}\right)\right)\right]
\end{aligned}
$$

## Continue

$$
\lambda_{a}=10^{-7}\left[\frac{I_{a}}{2} \frac{\mu}{\mu_{0}}+2 I_{a}\left(\ln \frac{D_{a x}}{r} \cdot \frac{D_{a n}}{D_{n x}}\right)\right)
$$

$$
\begin{aligned}
& +2 I_{b}\left(\ln \left(\frac{D_{b x}}{D_{a b}} \cdot \frac{D_{a n}}{D_{n x}}\right)\right) \\
& \left.+\ldots+2 I_{n-1}\left(\ln \left(\frac{D_{n-1 x}}{D_{a n-1}} \cdot \frac{D_{a n}}{D_{n x}}\right)\right)\right]
\end{aligned}
$$

## Continue

When X approaches infinity,

$$
\begin{aligned}
& \frac{D_{a x}}{D_{n x}}=\frac{D_{b x}}{D_{n x}}=\ldots \ldots . .=\frac{D_{n-1}}{D_{n x}}=1 \\
& \begin{aligned}
\lambda_{a}=10^{-7}\left[\frac{I_{a}}{2} \frac{\mu}{\mu_{0}}\right. & +2 I_{a} \ln \frac{D_{a n}}{r} \\
& +2 I_{b} \ln \frac{D_{a n}}{D_{a b}} \\
& \left.+\ldots+2 I_{n-1} \ln \frac{D_{a n}}{D_{a n-1}}\right]
\end{aligned}
\end{aligned}
$$

## Continue

Since, $-\ln A=\ln (A)^{-1}=\ln \frac{1}{A}$
$\lambda_{a}=10^{-7}\left[\frac{I_{a}}{2} \frac{\mu}{\mu_{0}}+2 I_{a} \ln \frac{1}{r}+2 I_{b} \ln \frac{1}{D_{a b}}\right.$
$+\ldots+2 I_{n-1} \ln \frac{1}{D_{a n-1}}$
$\left.+2 \ln D_{a n}\left(I_{a}+I_{b}+\ldots+I_{n-1}\right)\right]$

## Continue

$$
\begin{align*}
& \begin{array}{l}
\begin{array}{l}
\lambda_{a}=10^{-7}\left[\frac{I_{a}}{2} \frac{\mu}{\mu_{0}}+2 I_{a} \ln \frac{1}{r}+2 I_{b} \ln \frac{1}{D_{a b}}\right. \\
\\
\left.\quad+\ldots+2 I_{f} \ln \frac{1}{D_{a f}}+2 I_{n} \ln \frac{1}{D_{a n}}\right] \\
L_{a}=\frac{\lambda_{a}}{I_{a}} \quad \mathrm{~m} / \mathrm{H}
\end{array} \\
\mathrm{X}_{\mathrm{La}}=2 \pi f L_{a} \quad \Omega
\end{array}
\end{align*}
$$

## General Expression for Inductance of Two Parallel Conductors of Irregular Cross-Section



## Continue

The linkages about the small element I can be obtained by,

$$
\begin{aligned}
\lambda_{1}=2 * 1 \mathrm{O}^{-7} *\left(\frac{I}{\mathrm{n}}\right)\left(\frac{1}{4}\right. & +\ln \frac{1}{\mathrm{r}_{1}}+\ln \frac{1}{\mathrm{D}_{12}} \\
& +\ln \frac{1}{\mathrm{D}_{13}}+\ldots \\
& +\ln \frac{1}{\mathrm{D}_{1 \mathrm{n}}}-\ln \frac{1}{\mathrm{D}_{1 \mathrm{a}}} \\
& \left.-\ln \frac{1}{\mathrm{D}_{1 \mathrm{~B}}} \ldots-\ln \frac{1}{\mathrm{D}_{1 \mathrm{n}}}\right) \quad \text { Linkage } / m
\end{aligned}
$$

Similarly, $\lambda_{2}, \lambda_{3}, \ldots ., \lambda_{n}$ can be obtained
$\lambda_{\text {total }}=\lambda_{1}+\lambda_{2}+\lambda_{3}+\ldots \ldots+\lambda_{n}$

## he linkages about the conductor are gixen by

 ( $\lambda_{\text {total }}$ )$$
\begin{aligned}
\lambda_{\text {total }}=\frac{2 * 10^{-7}}{n^{2}} & I\left[\frac{1}{4}+\ln \frac{1}{r_{1}}+\ln \frac{1}{D_{12}}+\ldots+\ln \frac{1}{D_{1 n}}\right. \\
& +\frac{1}{4}+\ln \frac{1}{r_{2}}+\ln \frac{1}{D_{21}}+\ldots+\ln \frac{1}{D_{2 n}} \\
& +\frac{1}{4}+\ln \frac{1}{r_{n}}+\ln \frac{1}{D_{n 1}}+\ldots+\ln \frac{1}{D_{n n}} \\
& -\ln \frac{1}{D_{1 A}}-\ln \frac{1}{D_{1 B}}-\ldots-\ln \frac{1}{D_{1 n}} \\
& \left.-\ln \frac{1}{D_{2 A}}-\ln \frac{1}{D_{2 B}}-\ldots . . \ln \frac{1}{D_{2 n}}\right]
\end{aligned}
$$

## Continue

$$
\begin{aligned}
& \text { since } \ln \frac{1}{\mathrm{D}_{1}}-\ln \frac{1}{\mathrm{D}_{2}}=\ln \frac{1 / \mathrm{D}_{1}}{1 / \mathrm{D}_{2}}=\ln \frac{\mathrm{D}_{2}}{\mathrm{D}_{1}} \\
& \frac{1}{n^{2}} \ln X=\ln \sqrt[n^{2}]{X}
\end{aligned}
$$

## Continue

If n is taken as infinity, the term $\frac{1}{4 n}$ is negligible and approaches to zero, thus,

$$
\begin{aligned}
& \lambda=2 * 10^{-7} I \ln \frac{\sqrt[n^{2}]{D_{1 A} D_{1 B} \ldots \ldots . D_{1 n} D_{2 A} D_{2 B} \ldots D_{2 n} \ldots .}}{\sqrt[n^{2}]{r_{1} D_{12} \ldots . D_{1 n} r_{2} D_{21} \ldots \ldots \ldots \ldots D_{2 n} r_{n}}} \\
& \lambda=2 * 10^{-7} I \ln \frac{D_{m}}{D_{s}} \quad H / m
\end{aligned}
$$

$L=\frac{\lambda}{I}$

## Definitions:

$D_{m}$ : (Geometric mean distance) "GMD": is the distance between the one conductor in coil side and the other conductors in the other coil side.

Ds : (self - geo metric mean distance) "SGMD" or (Geometric mean radius )"GMR" is the distance between the one conductor in coil side and the other conductors in the same coil side

## Inductance of Two Parallel Wires with Single-Phase Circuit

$D_{m}=D$
$D_{s}=r e^{-0.25}$
$L=L_{a}+L_{b}$

Using general expression

H/m
(For both conductors )

## Inductance of Single-Phase Line with Multi-Conductors

using general expression
$L=2 * 10^{-7} \ln \frac{D_{m}}{D_{s}} \quad \mathrm{H} / \mathrm{m}$
For identical conductors, $\quad r_{a}=r_{b}=r_{x}=r_{y}=r$
$D_{m}=\sqrt[22^{2},]{D_{a x} \cdot D_{a y} \cdot D_{b x} \cdot D_{b y}}$
Where;
$D_{\text {ay }}=\sqrt{\left(D_{\text {ax }}\right)^{2}+\left(D_{\mathrm{xy}}\right)^{2}}$

## Continue

$$
\begin{array}{ll}
D_{s}=\sqrt[(2)]{2} \sqrt{r_{a} \cdot D_{a b} \cdot r_{b} \cdot D_{b a}}=\sqrt[4]{r_{a} D_{a b} r_{b} D_{b a}} \\
r_{a}=r_{b}=r & D_{a b}=D_{b a} \\
\text { Note }: r_{a}=r e^{-0.25} & D_{s}=\sqrt{r D_{a b}}
\end{array}
$$

If $D_{a b}=D_{x y}$, then $D_{s}$ of the conductors on the left-hand side as well as on the right-hand side is equal.

## With Our Best Wishes

Transmission and Distribution of Electrical Power Course Staff


